

# Network Systems and Kuramoto Oscillators

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2018 President, IEEE Control Systems Society  
A kind invitation to participate in CSS activities



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National Renewable Energy Laboratory, UCSB and University of Minnesota



## 1 Intro to Network Systems and Power Flow

### Known tests and a conjecture

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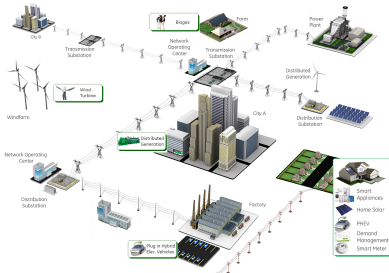
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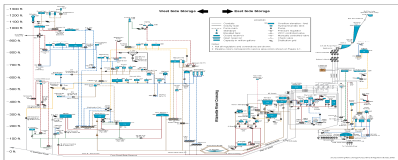
# Example network systems



Smart grid



Amazon robotic warehouse



Portland water network



Industrial chemical plant

# Linear network systems

$$x(k+1) = Ax(k) + b \quad \text{or} \quad \dot{x}(t) = Ax(t) + b$$



- 1 systems of interest
- 2 asymptotic behavior
- 3 tools

**network structure**  $\iff$  **function = asymptotic behavior**

# New text “Lectures on Network Systems”

## Lectures on Network Systems



Francesco Bullo

With contributions by  
Jorge Cortés  
Florian Dörfler  
Sonia Martínez

**Lectures on Network Systems**, 1 edition  
ISBN 978-1-986425-64-3

*For students: free PDF for download*

*For instructors: slides and answer keys*

<http://motion.me.ucsb.edu/book-lds>

<https://www.amazon.com/dp/1986425649>

300 pages (plus 200 pages solution manual)

3K downloads since Jun 2016

150 exercises with solutions

### Linear Systems:

- 1 social, sensor, robotic & compartmental examples,
- 2 matrix and graph theory, with an emphasis on Perron–Frobenius theory and algebraic graph theory,
- 3 averaging algorithms in discrete and continuous time, described by static and time-varying matrices, and
- 4 positive & compartmental systems, dynamical flow systems, Metzler matrices.

### Nonlinear Systems:

- 5 nonlinear consensus models,
- 6 population dynamic models in multi-species systems,
- 7 coupled oscillators, with an emphasis on the Kuramoto model and models of power networks

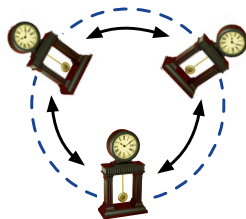
# Synchronization in Networks of Coupled Oscillators

Pendulum clocks & “*an odd kind of sympathy*”

[C. Huygens, Horologium Oscillatorium, 1673]

Today's canonical coupled oscillator model

[A. Winfree '67, Y. Kuramoto '75]



Coupled oscillator model:

$$\dot{\theta}_i = \omega_i - \sum_{j=1}^n a_{ij} \sin(\theta_i - \theta_j)$$

- **$n$  oscillators** with phase  $\theta_i \in \mathbb{S}^1$
- **non-identical** natural frequencies  $\omega_i \in \mathbb{R}^1$
- **coupling** with strength  $a_{ij} = a_{ji}$

# Synchronization in Networks of Coupled Oscillators

applications

## Coupled oscillator model:

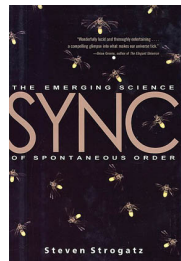
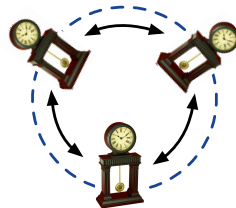
$$\dot{\theta}_i = \omega_i - \sum_{j=1}^n a_{ij} \sin(\theta_i - \theta_j)$$

## A few related applications:

- Sync in Josephson junctions  
[S. Watanabe et. al '97, K. Wiesenfeld et al. '98]
- Sync in a population of fireflies  
[G.B. Ermentrout '90, Y. Zhou et al. '06]
- Canonical model of coupled limit-cycle oscillators  
[F.C. Hoppensteadt et al. '97, E. Brown et al. '04]
- Countless sync phenomena in sciences/bio/tech.  
[A. Winfree '67, S.H. Strogatz '00, J. Acebrón '01]

citations on scholar.google:

Kuramoto oscillators 1.4K, synchronization



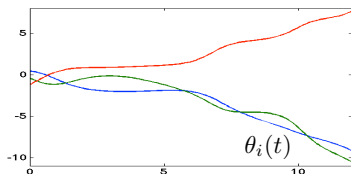


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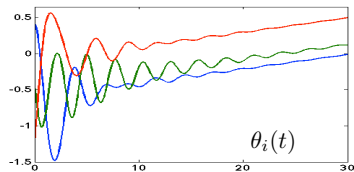
phenomenology and challenges

Function = synchronization

$$\dot{\theta}_i = \omega_i - \sum_{j=1}^n a_{ij} \sin(\theta_i - \theta_j)$$



coupling small &  $|\omega_i - \omega_j|$  large  
 $\Rightarrow$  incoherence = no sync



coupling large &  $|\omega_i - \omega_j|$  small  
 $\Rightarrow$  coherence = frequency sync

## Central question:

[S. Strogatz '01, A. Arenas et al. '08, S. Boccaletti et al. '06]

- loss of sync due to bifurcation
- trade-off “coupling” vs. “heterogeneity”
- how to quantify this trade-off

## 1 Intro to Network Systems and Power Flow

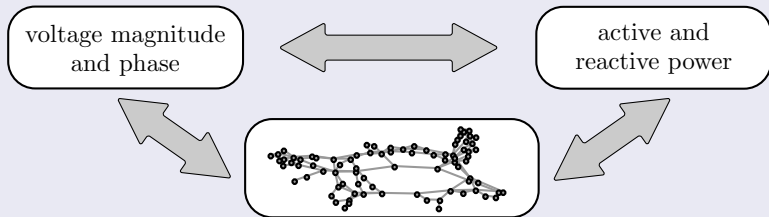
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# Power flow equations



- 1 secure operating conditions
- 2 feedback control
- 3 economic optimization

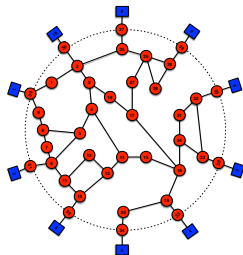
**network structure**



**function = power transmission**

# Power networks as quasi-synchronous AC circuits

- ① **generators** ■ and **loads** ●
- ② **physics:** Kirchoff and Ohm laws
- ③ today's simplifying assumptions:
  - ① **quasi-sync:** voltage and phase  $V_i, \theta_i$   
active and reactive power  $p_i, q_i$
  - ② lossless lines
  - ③ approximated decoupled equations



## Decoupled power flow equations

active: 
$$p_i = \sum_j a_{ij} \sin(\theta_i - \theta_j)$$

reactive: 
$$q_i = -\sum_j b_{ij} V_i V_j$$

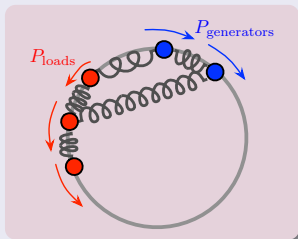
# Power Flow Equilibria

$$p_i = \sum_j a_{ij} \sin(\theta_i - \theta_j)$$

## As function of network structure/parameters

- 1 do equations admit solutions / operating points?
- 2 how much active power can network transmit / flow?
- 3 how to quantify stability margins?

## Active power dynamics and mechanical/spring analogy



### Coupled swing equations

$$m_i \ddot{\theta}_i + d_i \dot{\theta}_i = p_i - \sum_j a_{ij} \sin(\theta_i - \theta_j)$$

### Kuramoto coupled oscillators

$$\dot{\theta}_i = p_i - \sum_j a_{ij} \sin(\theta_i - \theta_j)$$

# Synchronization in Power Networks

**Sync is crucial** for the functionality and operation of the AC power grid. Generators have to swing in sync despite fluctuations/faults/contingencies.

**Given:** network parameters & topology and load & generation profile

**Q:** “ $\exists$  an optimal, stable, and robust synchronous operating point ?”

- ❶ Security analysis [Araposthatis et al. '81, Wu et al. '80 & '82, Ilić '92, ...]
- ❷ Load flow feasibility [Chiang et al. '90, Dobson '92, Lesieutre et al. '99, ...]
- ❸ Optimal generation dispatch [Lavaei et al. '12, Bose et al. '12, ...]
- ❹ Transient stability [Sastry et al. '80, Bergen et al. '81, Hill et al. '86, ...]
- ❺ Inverters in microgrids [Chandorkar et al. '93, Guerrero et al. '09, Zhong '11, ...]

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# Primer on algebraic graph theory

Weighted undirected graph with  $n$  nodes and  $m$  edges:

**Incidence matrix:**  $n \times m$  matrix  $B$  s.t.  $(B^\top p_{\text{active}})_{(ij)} = p_i - p_j$

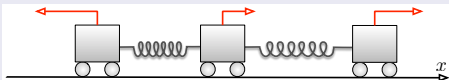
**Weight matrix:**  $m \times m$  diagonal matrix  $\mathcal{A}$

**Laplacian stiffness:**  $L = B\mathcal{A}B^\top$

**Kuramoto eq points:**  $p_{\text{active}} = B\mathcal{A} \sin(B^\top \theta)$

**Algebraic connectivity:**  $\lambda_2(L) = \text{second smallest eig of } L$

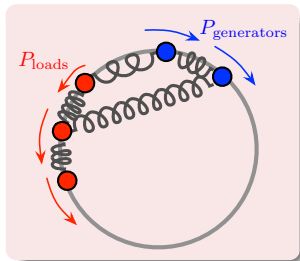
## Linear spring networks and $L^\dagger$



$$f_i = \sum a_{ij}(x_j - x_i) = -(Lx)_i$$
$$x = L^\dagger f \quad \text{for balanced } f \perp \mathbb{1}_n$$



# Known tests



Given balanced  $p_{\text{active}}$ , do angles exist?

$$p_{\text{active}} = B A \sin(B^T \theta)$$

synchronization arises if

**power transmission** < **connectivity strength**

Equilibrium angles (neighbors within  $\pi/2$  arc) exist if

$$\|B^T p_{\text{active}}\|_2 < \lambda_2(L) \quad \text{for unweighted graphs} \quad (\text{Old 2-norm } T)$$

$$\|B^T L^\dagger p_{\text{active}}\|_\infty < 1 \quad \text{for trees, complete} \quad (\text{Old } \infty\text{-norm } T)$$



at fixed radius and 2-norm, volume of ball  $\rightarrow 0^+$  as  $d \rightarrow +\infty$

# A standing conjecture

$\|B^\top L^\dagger p_{\text{active}}\|_\infty < 1$  appears to imply:

①  $\exists$  solution  $\theta^*$

②  $|\theta_i^* - \theta_j^*| \leq \arcsin(\|B^\top L^\dagger p_{\text{active}}\|_\infty)$  for all  $\{i, j\} \in \mathcal{E}$

Randomized test case (1000 instances)	Numerical worst-case angle differences: $\max_{\{i,j\} \in \mathcal{E}}  \theta_i^* - \theta_j^* $	Analytic prediction of angle differences: $\arcsin(\ B^\top L^\dagger p_{\text{active}}\ _\infty)$	Accuracy of condition: $\max_{\{i,j\} \in \mathcal{E}}  \theta_i^* - \theta_j^* $ $- \arcsin(\ B^\top L^\dagger p_{\text{active}}\ _\infty)$
9 bus system	0.12889 rad	0.12885 rad	$4.1218 \cdot 10^{-5}$ rad
IEEE 14 bus system	0.16622 rad	0.16594 rad	$2.7995 \cdot 10^{-4}$ rad
IEEE RTS 24	0.22309 rad	0.22139 rad	$1.7089 \cdot 10^{-3}$ rad
IEEE 30 bus system	0.1643 rad	0.16404 rad	$2.6140 \cdot 10^{-4}$ rad
New England 39	0.16821 rad	0.16815 rad	$6.6355 \cdot 10^{-5}$ rad
IEEE 57 bus system	0.20295 rad	0.18232 rad	$2.0630 \cdot 10^{-2}$ rad
IEEE RTS 96	0.24593 rad	0.245332 rad	$2.6076 \cdot 10^{-3}$ rad
IEEE 118 bus system	0.23524 rad	0.23464 rad	$5.9959 \cdot 10^{-4}$ rad
IEEE 300 bus system	0.43204 rad	0.43151 rad	$5.2618 \cdot 10^{-4}$ rad
Polish 2383 bus system	0.25144 rad	0.24723 rad	$4.2183 \cdot 10^{-3}$ rad

IEEE test cases: 50 % randomized loads and 33 % randomized generation

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Equilibrium angles (neighbors within  $\pi/2$  arc) exist if

$$\|B^\top p_{\text{active}}\|_2 < \lambda_2(L) \quad \text{for unweighted graphs} \quad (\text{Old 2-norm T})$$

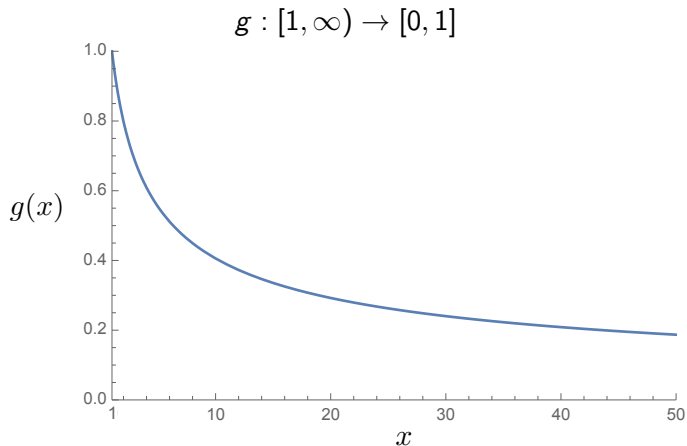
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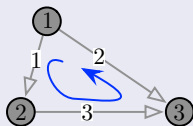
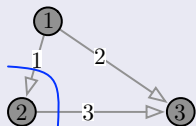
$$\|B^\top L^\dagger p_{\text{active}}\|_\infty < g(\|\mathcal{P}\|_\infty) \quad \text{for all graphs} \quad (\text{New } \infty\text{-norm T})$$

where  $g$  is monotonically decreasing



$$g(x) = \frac{y(x) + \sin(y(x))}{2} - x \frac{y(x) - \sin(y(x))}{2} \Big|_{y(x)=\arccos(\frac{x-1}{x+1})}$$

and where  $\mathcal{P}$  is a projection



$$\underbrace{\mathbb{R}^m}_{\text{edge space}} = \underbrace{\text{Im}(B^\top)}_{\text{cutset space}} \oplus \underbrace{\text{Ker}(BA)}_{\text{weighted cycle space}}$$

$$\mathcal{P} = B^\top L^\dagger BA = \text{oblique projection onto } \text{Im}(B^\top) \\ \text{parallel to } \text{Ker}(BA)$$

(recall: orthogonal projector onto  $\text{Im}(C)$  is  $C(C^\top C)^{-1}C^\top$  for full rank  $C$ )

- ❶ if  $G$  unweighted, then  $\mathcal{P}$  is orthogonal and  $\|\mathcal{P}\|_2 = 1$
- ❷ if  $G$  acyclic, then  $\mathcal{P} = I_m$  and  $\|\mathcal{P}\|_p = 1$
- ❸ if  $G$  uniform complete or ring, then  $\|\mathcal{P}\|_\infty = 2(n-1)/n \leq 2$

# Unifying Theorem

Equilibrium angles (neighbors within  $\gamma$  arc) exist if, in some  $p$ -norm,

$$\|B^\top L^\dagger p_{\text{active}}\|_p \leq \gamma \alpha_p(\gamma) \quad \text{for all graphs} \quad (\text{New } p\text{-norm T})$$

$$\alpha_p(\gamma) := \min \text{ amplification factor of } \mathcal{P}[\text{sinc}(x)]$$

For unweighted  $p = 2$ , new test sharper than old

$$\|B^\top L^\dagger p_{\text{active}}\|_2 \leq \sin(\gamma) \quad (\text{New 2-norm T})$$

For  $p = \infty$ , new test is for all graphs

$$\|B^\top L^\dagger p_{\text{active}}\|_\infty \leq g(\|\mathcal{P}\|_\infty) \quad (\text{New } \infty\text{-norm T})$$

# Comparison of sufficient and approximate sync tests

$K_c$  = critical coupling of Kuramoto model, computed via MATLAB *fsolve*

$K_T$  = smallest value of scaling factor for which test T fails

Test Case	Critical ratio $K_T/K_c$				
	old 2-norm conjectured	new 2-norm conjectured	new $\infty$ -norm	old $\infty$ -norm approximate	$\alpha_\infty$ test <i>fmincon</i>
IEEE 9	16.54 %	59.06 %	73.74 %	92.13 %	85.06 % <sup>†</sup>
IEEE 14	8.33 %	42.27 %	59.42 %	83.09 %	81.32 % <sup>†</sup>
IEEE RTS 24	3.86 %	35.62 %	53.44 %	89.48 %	89.48 % <sup>†</sup>
IEEE 30	2.70 %	40.98 %	55.70 %	85.54 %	85.54 % <sup>†</sup>
IEEE 39	2.97 %	37.32 %	67.57 %	100 %	100 % <sup>†</sup>
IEEE 57	0.36 %	31.93 %	40.69 %	84.67 %	— <sup>*</sup>
IEEE 118	0.29 %	24.61 %	43.70 %	85.95 %	— <sup>*</sup>
IEEE 300	0.20 %	24.13 %	40.33 %	99.80 %	— <sup>*</sup>
Polish 2383	0.11 %	13.93 %	29.08 %	82.85 %	— <sup>*</sup>

<sup>†</sup> *fmincon* has been run for 100 randomized initial phase angles.

<sup>\*</sup> *fmincon* does not converge.



## Proof sketch 1/2: Rewriting the equilibrium equation

For what  $B, \mathcal{A}, p_{\text{active}}$  does there exist  $\theta$  solution to:

$$p_{\text{active}} = B\mathcal{A}\sin(B^{\top}\theta)$$

For what projection  $\mathcal{P}$  and flow  $z$  in cutset space,  
does there exist  $x$  in cutset spacesolution to:

$$\begin{aligned} z = \mathcal{P}\sin(x) &\iff z = \mathcal{P}[\text{sinc}(x)]x \\ &\iff x = (\mathcal{P}[\text{sinc}(x)])^{-1}z =: h(x) \end{aligned}$$

# Proof sketch 2/2: Amplification factor & Brouwer fixed point thm

- ① look for  $x$  solving

$$x = h(x) = (\mathcal{P}[\text{sinc}(x)])^{-1}z$$

- ② take  $p$  norm, define **min amplification factor** of  $\mathcal{P}[\text{sinc}(x)]$ :

$$\alpha_p(\gamma) := \min_{\|x\|_p \leq \gamma} \min_{\|y\|_p = 1} \|\mathcal{P}[\text{sinc}(x)]y\|_p$$

If  $\|z\|_p \leq \gamma \alpha_p(\gamma)$  and  $x \in \mathcal{B}_p(\gamma) = \{x \mid \|x\|_p \leq \gamma\}$ , then

$$\begin{aligned} \|h(x)\|_p &\leq \max_x \max_y \|(\mathcal{P}[\text{sinc}(x)])^{-1}y\|_p \cdot \|z\|_p \\ &\leq \frac{\|z\|_p}{\alpha_p(\gamma)} \leq \gamma \end{aligned}$$

hence  $h(x) \in \mathcal{B}_p(\gamma)$  and  $h$  satisfies Brouwer on  $\mathcal{B}_p(\gamma)$

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# Computational method via power series

Given  $z$ , compute  $x$  solution to

$$z = \mathcal{P} \sin(x)$$

Assume  $x = \sum_{i=0}^{\infty} A_{2i+1}(z)$ , where  $A_{2i+1}(z)$  is homogeneous degree  $2i+1$

$$z = \mathcal{P} \sum_{k=0}^{\infty} \frac{(-1)^k}{(2k+1)!} x^{\circ 2k+1} = \mathcal{P} \sum_{k=0}^{\infty} \frac{(-1)^k}{(2k+1)!} \left( \sum_{i=0}^{\infty} A_{2i+1}(z) \right)^{\circ 2k+1}$$

Equate left-hand and right-hand side at order  $1, 3, \dots, 2j+1$ :

$$A_1(z) = z$$

$$A_{2j+1}(z) = \mathcal{P} \left( \sum_{k=1}^j \frac{(-1)^{k+1}}{(2k+1)!} \sum_{\substack{\text{odd } \alpha_1, \dots, \alpha_{2k+1} \text{ s.t.} \\ \alpha_1 + \dots + \alpha_{2k+1} = 2j+1}} A_{\alpha_1}(z) \circ \dots \circ A_{\alpha_{2k+1}}(z) \right)$$

### Step 3: Series expansion for inverse Kuramoto map

Unique solution to  $z = \mathcal{P} \sin(x)$  is

$$x = \sum_{i=0}^{\infty} A_{2i+1}(z)$$

$$A_1(z) = z = B^\top L^\dagger p_{\text{active}}$$

$$A_3(z) = \mathcal{P}\left(\frac{1}{3!} z^{\circ 3}\right)$$

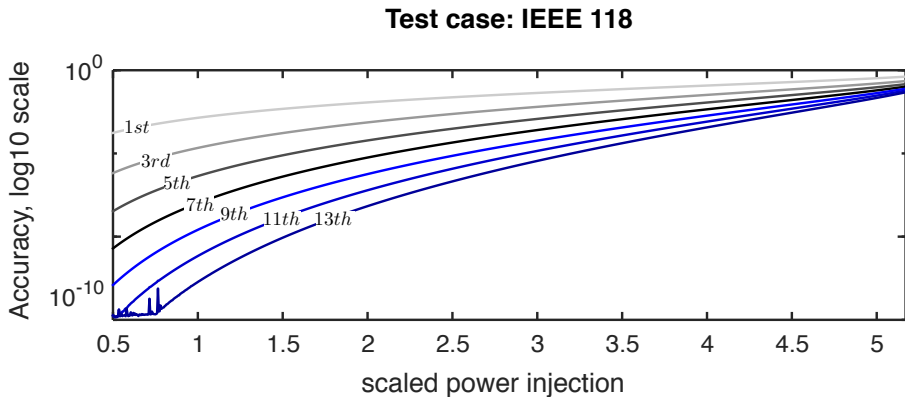
$$A_5(z) = \mathcal{P}\left(\frac{3}{3!} A_3(z) \circ z^{\circ 2} - \frac{1}{5!} z^{\circ 5}\right)$$

$$A_7(z) = \mathcal{P}\left(\frac{3}{3!} A_5(z) \circ z^{\circ 2} + \frac{3}{3!} A_3(z)^{\circ 2} \circ z - \frac{5}{5!} A_3(z) \circ z^{\circ 4} + \frac{1}{7!} z^{\circ 7}\right)$$

arbitrary higher-order terms can be computed symbolically

For sufficiently small  $\|z\|_p$ , series converges uniformly absolutely

# Numerical examples



# Kuramoto Oscillators and Power Flow

## New physical insight

- 1 sharp sufficient conditions for equilibria
  - upper bounds on transmission capacity
  - stability margins as notions of distance from bifurcations
- 2 new computational methods via power series

## Applications

- 1 secure operating conditions: (Dörfler et al, PNAS '13)
- 2 feedback control: (Simpson-Porco et al, TIE '15)
- 3 economic optimization: (Todescato et al, TCNS '17)

## Future research

- 1 close the gap between sufficient and necessary conditions
- 2 more realistic coupled power flow equations
- 3 applications to other flow networks (water, gas ...)