

Contraction Theory of Output Regulation

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Contraction Theory for Systems, Control, Optimization, and Learning
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Outline

- 1 Introduction
- 2 The Linear Case
- 3 Forwarding Design
- 4 Integral Action and Contraction
- 5 Conclusions

Outline

1 Introduction

2 The Linear Case

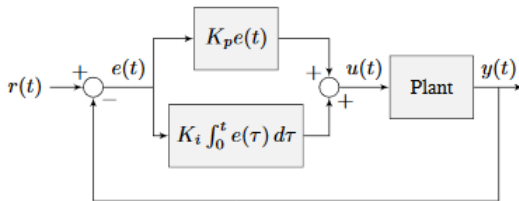
3 Forwarding Design

4 Integral Action and Contraction

5 Conclusions

Introduction to Integral Action

- Goal of feedback: achieve a prescribed goal in presence of model uncertainties
- For set-point tracking: P, PI, PID
- Example of standard PI controller:



- Taught in any basic course of control
- Industrial applications

Some milestones

1868: James Clerk Maxwell: “On Governors”

Scottish physicist and mathematician

1911: Elmer Ambrose Sperry: PID controller using a marine gyro compass for automatic steering of ships.

American inventor and entrepreneur

1922: Minorsky: “Directional stability of automatically steered bodies”

American mathematician

“the second class of controllers (= PI) has the remarkable result that such a (constant) disturbance has no influence upon the device”

1931: Foxboro, USA (Schneider Electric Company since 2014): pneumatic differential PI controller named Stabilog Model 10

1942: Ziegler-Nichols method for optimal tuning of a PID controller

Output Regulation Theory

Integral action as a special case of robust output regulation (servomechanism problem)

$$\begin{aligned}\dot{w} &= Sw & w : \text{perturbations and references} \\ \dot{x} &= Ax + Bu + Pw \\ e &= Cx + Qw\end{aligned}$$

Regulation objective: $\lim_{t \rightarrow \infty} e(t) = 0$

1976: Francis, Wohnam and Davison: the internal model principle

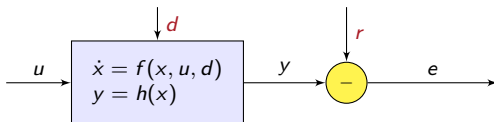
“the output regulation property is insensitive to plant parameter variations only if the controller utilizes feedback of the regulated variable, and incorporates in the feedback path a suitably reduplicated model of the dynamic structure of the exogenous signals which the regulator is required to process”

⇒ Necessity and Sufficiency of an integral action for set-point tracking and constant perturbation rejection

- The adjective “robust” has a different meaning w.r.t. to robust control theory

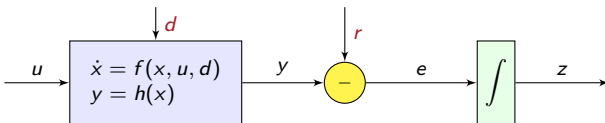
From 80's: Development of nonlinear output regulation theory

How the Integral Action works



- x : state
- u : control
- e : regulated output
- (r, d) : constant references and perturbations

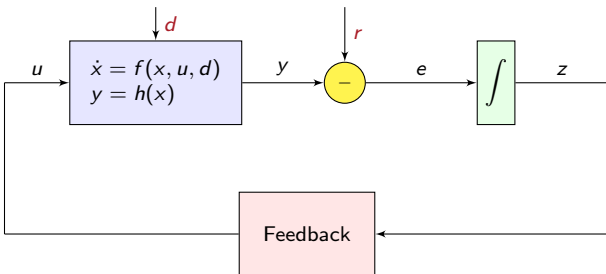
How the Integral Action works



- 1 Add the integral action on the regulated output e
- 2 Design a feedback so that the for a given pair (r, d) , the closed-loop system admits an asymptotically stable equilibrium (x°, z°)
- 3 On the equilibrium (x°, z°) , we have

$$0 = \dot{z} = e \quad \iff h(x^\circ) = r$$

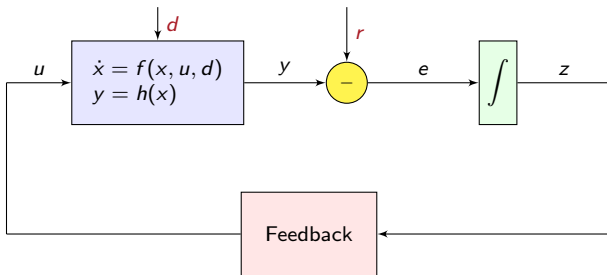
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Main difficulties

- Design of a stabilizing feedback for the extended system (x, z) to guarantee the existence of an **equilibrium**
 - domain of attraction (DoA)?
 - uniformity with respect to (d, r) ?

- Persistence of an **equilibrium** in presence of model uncertainties Δ_f, Δ_h

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Revising the linear approach

Consider the linear system

$$\begin{cases} \dot{x} = Ax + Bu + d & x \in \mathbb{R}^n, u \in \mathbb{R}^m \\ e = Cx - r & e \in \mathbb{R}^p \end{cases}$$

Theorem

Suppose that

- (A, B) is stabilizable;
- non-resonance condition $\text{rank} \begin{pmatrix} A & B \\ C & 0 \end{pmatrix} = n + p$ holds¹.

Then, there exists K, L such that the controller

$$\begin{cases} \dot{z} = e \\ u = Kx + Lz \end{cases}$$

solves the robust output regulation problem, i.e. $\lim_{t \rightarrow \infty} e(t) = 0$ for all initial conditions $(x_0, z_0) \in \mathbb{R}^n \times \mathbb{R}^p$, all constant references and disturbances (r, d) and for small model perturbations $\Delta_A, \Delta_B, \Delta_C$.

¹This conditions is equivalent to ask that the transfer function between u and e has no zeros at the origin.

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Sketch of the proof (1)

- (A, B) stabilizable and the non-resonance condition implies the extended system

$$\left(\begin{pmatrix} A & 0 \\ C & 0 \end{pmatrix}, \begin{pmatrix} B \\ 0 \end{pmatrix} \right)$$

is stabilizable, i.e., there exists K, L so that $F := \begin{pmatrix} A + BK & BL \\ C & 0 \end{pmatrix}$ is Hurwitz.

- For any (d, r) , the system

$$\begin{cases} \dot{x} = (A + BK)x + BLz + d \\ \dot{z} = Cz - r \end{cases}$$

admits an equilibrium (x°, z°) given by

$$0 = \begin{pmatrix} A + BK & BL \\ C & 0 \end{pmatrix} \begin{pmatrix} x^\circ \\ z^\circ \end{pmatrix} + \begin{pmatrix} d \\ -r \end{pmatrix} \implies \begin{pmatrix} x^\circ \\ z^\circ \end{pmatrix} = F^{-1} \begin{pmatrix} d \\ -r \end{pmatrix}$$

- This equilibrium (x°, z°) is GAS due to the stability of F . This can be shown in error coordinates $(x - x^\circ, z - z^\circ)$.

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- Note that if

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is Hurwitz, for small perturbations $\Delta_A, \Delta_B, \Delta_C$, stability of

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is preserved..

.. and so the existence of a stable equilibrium on which $e = 0$!

⇒ The design is **robust** and asymptotic regulation is preserved in presence of **model uncertainties!**

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Takeaway message from linear world

Linear lesson:

- The design of the feedback is independent of (d, r)
- Stability guarantees the existence of a unique equilibrium for any (d, r) and in presence of model uncertainties

Question:

- Can we extend such a paradigm to the nonlinear ODEs?

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A Stabilization of cascade systems

- Consider a system of the form

$$\begin{cases} \dot{x} = f(x) + g(x)u \\ \dot{z} = h(x) \end{cases}$$

- **Problem:** design a feedback $u = \alpha(x, z)$ guaranteeing origin GAS (and LES)

- **A possible solution:** forwarding design

see, e.g., Praly, Mazenc, A. Astolfi, Ortega, Teel, Sepulchre, Kokotovic, Kristic, ..

- **Remark:** a necessary condition for the existence of α is the existence of a α_0 :

$$\dot{x} = f(x) + g(x)\alpha_0(x) \quad \text{is GAS}$$

In the following we suppose this step has already been done:

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Forwarding design: main ideas

- Consider a system of the form

$$\begin{cases} \dot{x} = f(x) + g(x)u \\ \dot{z} = h(x) \end{cases}$$

- Let x be the fast stable dynamics and z the slow one
- If the origin of $\dot{x} = f(x)$ is GAS and LES, we can define an **invariant-manifold** for $z = M(x)$ satisfying

$$L_f M(x) := \frac{\partial M}{\partial x}(x) f(x) = h(x)$$

- Consider the change of coordinates $\zeta := z - M(x)$ giving-

$$\begin{cases} \dot{x} = f(x) + g(x)u \\ \dot{\zeta} = -L_g M(x)u \end{cases}$$

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Forwarding design: main ideas (2)

- We have

$$\begin{cases} \dot{x} = f(x) + g(x)u \\ \dot{\zeta} = -L_g M(x)u \end{cases}$$

- With the Lyapunov function $W(x, \zeta) = V(x) + \frac{1}{2}\zeta^2$ we obtain

$$\dot{W} \leq L_f V(x) + (L_g V(x) - \zeta L_g M(x)) u$$

⇒ Select $u = -(L_g V(x) - \zeta L_g M(x))$ to obtain a negative derivative

- We obtain

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- If $L_g M(0) \neq 0$ we can conclude stability of the origin $(x, \zeta) = 0$.

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Forwarding design: main result

Lemma (Existence of the Invariant Manifold)

Suppose

- The origin of $\dot{x} = f(x)$ is GAS and LES, $f(0) = 0$, $h(0) = 0$
- The non-resonance condition $CA^{-1}B \neq 0$ holds, with

$$A := \frac{\partial f}{\partial x}(0), \quad B := g(0), \quad C := \frac{\partial h}{\partial x}(0).$$

Then, there exists a C^2 function M satisfying $M(0) = 0$, $\frac{\partial M}{\partial x}(0) = CA^{-1}$ and ²

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Theorem (Forwarding Stabilization)

There exists a feedback $u = \alpha(x, z)$ such that the origin of

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² $L_g M(0)$ is the DC-gain at the origin of $\dot{x} = f(x) + g(x)u$, $y = h(x)$.

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Forwarding and perturbations

Consider now the perturbed system:

$$\begin{aligned}\dot{x} &= f(x, d) + g(x, d)\alpha(x, z) \\ \dot{z} &= h(x, r)\end{aligned}$$

with α designed with the forwarding as shown before.

- When $(d, r) = 0$ then the origin is GAS and LES
- Can we conclude the existence of an equilibrium for $(d, r) \neq 0$?
- In general, only for small values, i.e. $|(d, r)| \leq \varepsilon$

Total stability: equilibria are preserved under small perturbations

[Astolfi Praly, TAC 2017]

- To achieve global results, we need stronger properties:

⇒ Contraction

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Towards the existence of a “global” controller

- Consider again the closed-loop system and use a compact notation

$$\begin{cases} \dot{x} = f(x, \alpha(x, z), d) \\ \dot{z} = h(x) - r \end{cases} \quad \Longrightarrow \quad \dot{\xi} = F(\xi, (d, r))$$

- Global regulation can be obtained if the vector field F admits a fixed point for any (d, r)
- **Main Idea:** use Banach fixed point theorem..
 \Longrightarrow we need F to be a (uniform) contraction

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Some highlights on Contraction Theory

Contraction with Riemannian metric

The vector field $F : \mathbb{R}^n \rightarrow \mathbb{R}^n$ is contracting if (and only if, for F C^2 globally Lipschitz) there exists a (Riemannian) metric $P : \mathbb{R}^n \rightarrow \mathbb{R}^{n \times n}$ taking SPD values and $\underline{p}, \underline{q} > 0$ such that³

$$\underline{p}I \leq P(\xi) \leq \bar{p}I, \quad L_F P(\xi) := \dot{P}(\xi) + P(\xi) \frac{\partial F}{\partial \xi}(\xi) + \frac{\partial F}{\partial \xi}(\xi)^\top P(\xi) \preceq -qI, \quad \forall \xi \in \mathbb{R}^n.$$

Remark: generalization of Lyapunov Matrix Inequality $PA + A^\top P \preceq -Q$

Contraction and Incremental Stability

Suppose F is a contraction. Then $\exists k, \lambda > 0$ such that solutions to system $\dot{\xi} = F(\xi)$ satisfy

$$|\phi(\xi_a, t) - \phi(\xi_b, t)| \leq k |\xi_a - \xi_b| \exp(-\lambda t) \quad \forall \xi_a, \xi_b \in \mathbb{R}^n.$$

In other words, the system is Incrementally Globally Exponentially Stable (δ GES).

³The notation \dot{P} defines a matrix with its ij -th elements defined as $\dot{P}_{ij} = \frac{\partial P_{ij}}{\partial \xi} F(\xi)$

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Contraction and equilibria

Incremental Stability and Equilibria

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Then there exists a unique equilibrium $\xi^o \in \mathbb{R}^n$ which is globally exponentially stable.

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Sketch of the proof:

- Select τ such that $k \exp(-\lambda\tau) < 1$.
- The application $\xi \mapsto \phi(\xi, \tau)$ defines a **contraction**:

$$|\phi(\xi_a, \tau) - \phi(\xi_b, \tau)| < |\xi_a - \xi_b| \quad \forall \xi_a, \xi_b \in \mathbb{R}^n.$$

- **Banach fixed point theorem** gives existence and uniqueness of ξ° .

Contraction and equilibria

Incremental Stability and Equilibria

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Then there exists a unique equilibrium $\xi^o \in \mathbb{R}^n$ which is globally exponentially stable.

In order to apply previous theorem we need the system

$$\begin{cases} \dot{x} = f(x, \alpha(x, z), d) \\ \dot{z} = h(x) - r \end{cases} \iff \dot{\xi} = F(\xi, (d, r))$$

to be δ GES **uniformly** in (d, r) .

\implies we need a **uniform contraction**

$$\dot{P}(\xi, (d, r)) + P(\xi) \frac{\partial F}{\partial \xi}(\xi, (d, r)) + \frac{\partial F}{\partial \xi}(\xi, (d, r))^\top P(\xi) \leq -qI \quad \forall \xi, (d, r)$$

Killing vector and uniform contraction

Killing vector

Given a 2-tensor $P : \mathbb{R}^n \rightarrow \mathbb{R}^{n \times n}$, a C^1 function $G : \mathbb{R}^n \rightarrow \mathbb{R}^m$ is said to be a Killing vector for P if $L_G P(\xi) = 0$ for all $\xi \in \mathbb{R}^n$.

- Consider a system

$$\dot{\xi} = F(\xi) + G(\xi)w$$

- Suppose there exist a P such that that

- F is contractive w.r.t P : $L_F P(\xi) \preceq -qI$
- G is a Killing vector for P : $L_G P(\xi) = 0$

- Then,

$$L_F P(\xi) + L_G P(\xi) w \preceq -qI \quad \forall \xi, w$$

\implies the system defines a uniform contraction \implies is δ GES uniformly $\forall w!$

Problem: design of the feedback $\alpha(x, z)$ satisfying previous conditions

Killing vector and uniform contraction

Killing vector

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Sufficient conditions for contractive forwarding

Consider the system

$$\begin{cases} \dot{x} = f(x) + g(x)(u + d) \\ \dot{z} = h(x) - r \end{cases}$$

Theorem (Incremental Uniform Global Forwarding Stabilization)

Suppose that

- f is contraction⁴ for P and g is a Killing for P
- there exists a function $M : \mathbb{R}^n \rightarrow \mathbb{R}$ and a constant $\gamma > 0$ satisfying

$$L_f M(x) = h(x), \quad L_g M(x) = \gamma$$

Then, for any $k > 0$ the control law

$$u = k [z - M(x)]$$

makes the closed-loop system **uniformly contractive** and $\lim_{t \rightarrow \infty} h(x) = r$ for any initial condition $(x_0, z_0) \in \mathbb{R}^n \times \mathbb{R}$ and any (d, r) .

[Giaccagli, Astolfi Andrieu, Marconi, TAC 2022]

⁴This can be also obtained after a preliminary state-feedback with Control Contraction Metrics:

$$L_f P(x) + P(x)g(x)g(x)^\top P(x) \preceq -qI$$

Some Remarks

- The first conditions corresponds to the **stabilizability** of (A, B) in the proposed contractive framework
 - The second condition correspond to a **global uniform non-resonance condition**, i.e., a controllability (contractive) condition for the extended system (x, z)
 - Design based on the construction of a **contraction metric** for the closed-loop dynamics
- ✓ The control law depends on the solution of a PDE

$$L_f M(x) = h(x)$$

but there exist alternative designs to rely only on an approximation of M

- ✗ Conditions are restrictive due to the nature of the problem we aim at solving:
⇒ The result is global in the initial conditions and in (d, r)
- ✗ We considered only disturbances d satisfying a **matching-condition**

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Outline

1 Introduction

2 The Linear Case

3 Forwarding Design

4 Integral Action and Contraction

5 Conclusions

Conclusions

Takeaway messages:

- We proposed sufficient conditions for the design of a **global integral action** based on **forwarding and contraction analysis**
- Integral action has many applications: PI-control, tracking, and also optimization

$$\begin{array}{l} \min f(x) \\ Ax = b \end{array} \quad \Longrightarrow \quad \begin{array}{l} \dot{x} = \nabla f(x) - A^\top \lambda \\ \dot{\lambda} = Ax - b \end{array}$$

16:30–16:55: Time-Varying Convex Optimization: A Contraction and Equilibrium Tracking Approach, Francesco Bullo

- Possible extension to **periodic references/disturbances** and **harmonic regulation** (no time in this presentation)

$$\begin{array}{ll} \dot{x} = f(x) + g(x)(u + d(t)) & d(t+T) = d(t) \\ e = h(x) - r(t) & r(t+T) = r(t) \end{array}$$

[Giaccagli, Astolfi Andrieu, Marconi, TAC 2024]

Conclusions (2)

Open Problems:

- Can we relax δ GES with δ GAS to ensure the existence of an equilibrium?

Kato, Astolfi, Andrieu, Praly, ‘‘Incremental global asymptotic stability equals incremental global exponential stability - but at equilibria’’, NOLCOS 2025

- Is the Killing vector condition necessary for global uniform contractions?

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- Can we relax contraction with 2-contraction to ensure the existence of an equilibrium?

Giaccagli, Lorenzetti, Astolfi, Andrieu, ‘‘PI-control for non-linear systems with multiple equilibria via 2-contraction’’, NOLCOS 2025

what is 2-contraction?

11:00–11:25: On 2-Contraction and Non-Oscillatory Systems: Some Theory and Applications, David Angeli.

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Thanks and references



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